

Plane Waves and Planar Boundaries in FDTD Simulations

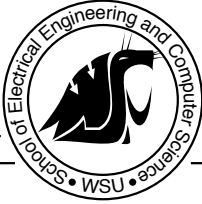


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Motivation/Overview

Maxwell's equations (continuous world):

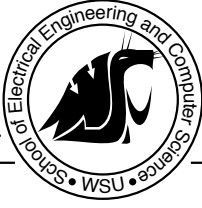
- Simple problems are easy to solve
- Complex problems are hard to solve

Yee FDTD method (discrete world):

- Complex problems are easy to solve
- Simple problems are relatively hard to solve

Solutions to simple problems can yield insight into performance and limits of numerical algorithms. Addressed in this talk:

- Orthogonality of $\bar{\mathbf{E}}$, $\bar{\mathbf{H}}$, and $\tilde{\mathbf{k}}$
- Characteristic impedance
- Reflection coefficient from planar boundaries



Yee Algorithm

Forgy notation[†]:

$$\begin{aligned}\bar{\mathbf{S}}^+ s_t^+ \partial_t \epsilon \bar{\mathbf{E}}^{\bar{m}} &= \bar{\mathbf{S}}^+ s_t^+ \bar{\mathbf{C}} \bar{\mathbf{H}}^{\bar{m}} \\ -\bar{\mathbf{S}}^- s_x^+ s_y^+ s_z^+ \partial_t \mu \bar{\mathbf{H}}^{\bar{m}} &= \bar{\mathbf{S}}^- s_x^+ s_y^+ s_z^+ \bar{\mathbf{C}} \bar{\mathbf{E}}^{\bar{m}}\end{aligned}$$

where s_i^+ shifts i th index by 1/2 and

$$\bar{\mathbf{S}}^+ = \begin{bmatrix} s_x^+ & 0 & 0 \\ 0 & s_y^+ & 0 \\ 0 & 0 & s_z^+ \end{bmatrix} \quad \text{and} \quad \bar{\mathbf{C}} = \begin{bmatrix} 0 & -\partial_z & \partial_y \\ \partial_z & 0 & -\partial_x \\ -\partial_y & \partial_x & 0 \end{bmatrix}$$

Assume plane-wave propagation:

$$\bar{\mathbf{E}}^{\bar{m}} = \bar{\mathbf{E}}_0 e^{j(\omega m_t \Delta_t - \tilde{k}_x m_x \Delta_x - \tilde{k}_y m_y \Delta_y - \tilde{k}_z m_z \Delta_z)}.$$

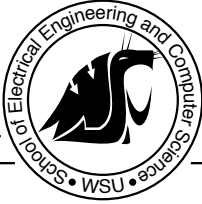
where numeric wave vector given by:

$$\tilde{\mathbf{k}} = [\tilde{k}_x, \tilde{k}_y, \tilde{k}_z] = \tilde{k} [\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta]$$

Finite-difference operators become

$$\begin{aligned}\partial_i \bar{\mathbf{E}}^{\bar{m}} &= -j \frac{2}{\Delta_i} \sin \left(\frac{\tilde{k}_i \Delta_i}{2} \right) \bar{\mathbf{E}}^{\bar{m}} = -j K_i \bar{\mathbf{E}}^{\bar{m}} \\ \partial_t \bar{\mathbf{E}}^{\bar{m}} &= j \frac{2}{\Delta_t} \sin \left(\frac{\omega \Delta_t}{2} \right) \bar{\mathbf{E}}^{\bar{m}} = j \Omega \bar{\mathbf{E}}^{\bar{m}}\end{aligned}$$

[†]E. A. Forgy, Master's Thesis, UIUC, 1998



Orthogonality

In source-free region, Yee grid divergence-free[†]:

$$\begin{aligned}\tilde{\nabla} \cdot \bar{\mathbf{E}}^{\bar{m}} &= 0 & \Leftrightarrow & \quad -j\bar{\mathbf{K}} \cdot \bar{\mathbf{E}}^{\bar{m}} = 0 \\ \tilde{\nabla} \cdot \bar{\mathbf{H}}^{\bar{m}} &= 0 & \Leftrightarrow & \quad -j\bar{\mathbf{K}} \cdot \bar{\mathbf{H}}^{\bar{m}} = 0\end{aligned}$$

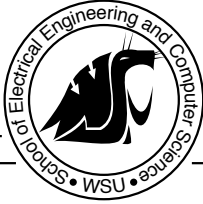
where $\tilde{\nabla} = [\partial_x, \partial_y, \partial_z]$.

Curl operator can be expressed in terms of $\bar{\mathbf{K}}$. Yee algorithm dictates

$$\begin{aligned}j\Omega\epsilon\bar{\mathbf{E}}^{\bar{m}} &= -j\bar{\mathbf{K}} \times \bar{\mathbf{H}}^{\bar{m}}, \\ -j\Omega\mu\bar{\mathbf{H}}^{\bar{m}} &= -j\bar{\mathbf{K}} \times \bar{\mathbf{E}}^{\bar{m}}.\end{aligned}$$

$\bar{\mathbf{E}}$, $\bar{\mathbf{H}}$, and $\bar{\mathbf{K}}$ are mutually orthogonal.
However, $\bar{\mathbf{K}}$ not necessarily parallel to $\tilde{\mathbf{k}}$
(direction of wave propagation).

[†]A. Taflove and S. Hagness, *Computational Electrodynamics*, pp. 96–98, 2000



Angle between $\bar{\mathbf{K}}$ and $\tilde{\mathbf{k}}$

Using dispersion relation, one can solve for angle between $\bar{\mathbf{K}}$ and $\tilde{\mathbf{k}}$.

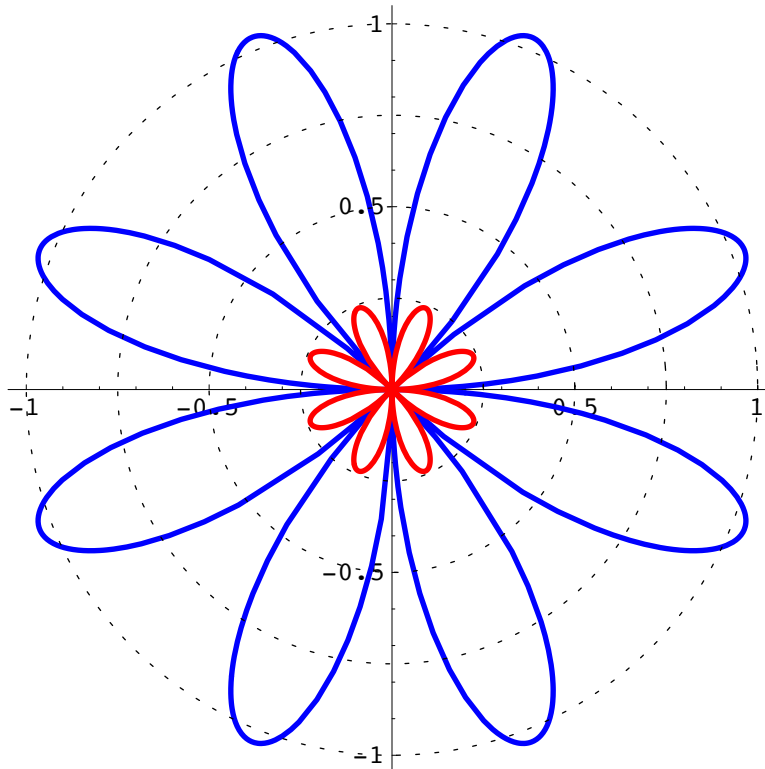
Angle is function of direction of propagation, discretization, and Courant number (weakly).

Courant number: $1/\sqrt{3}$

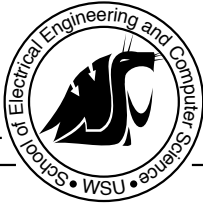
Discretization: 5 or 10 cells/ λ

$$\tilde{\mathbf{k}} = \tilde{k}[\cos \phi, \sin \phi, 0]$$

Angle between \mathbf{K} and $\tilde{\mathbf{k}}$ [degrees]



⇒ Second-order behavior

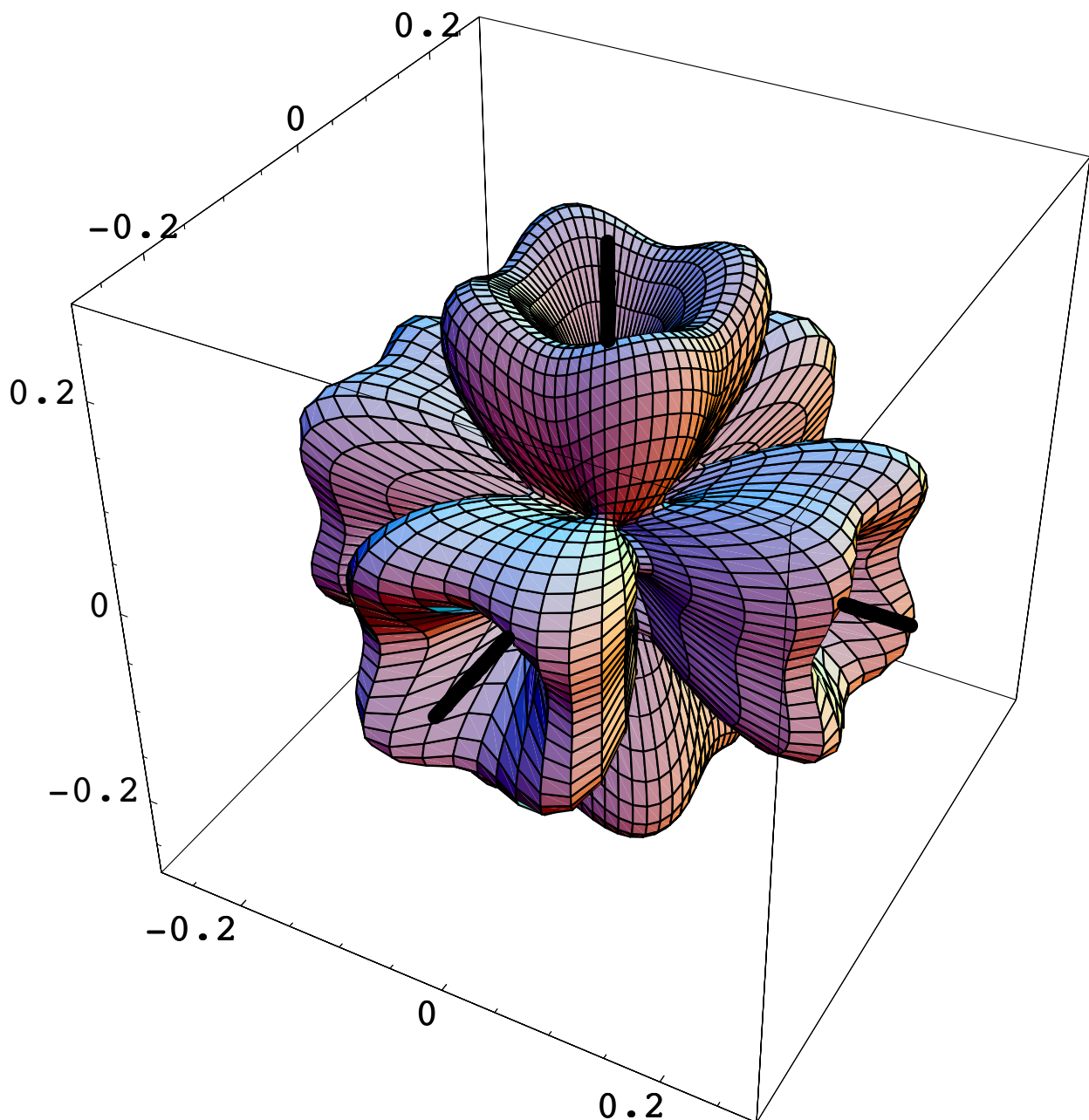


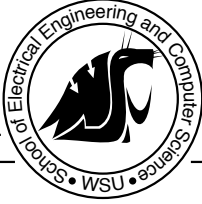
Angle between $\bar{\mathbf{K}}$ and $\tilde{\mathbf{k}}$: 3D

Courant number: $1/\sqrt{3}$

Discretization: 10 cells/ λ

Angle between $\bar{\mathbf{K}}$ and $\tilde{\mathbf{k}}$ [degrees]





Characteristic Impedance

Take magnitude of both sides of governing equation:

$$|j\Omega\epsilon\bar{\mathbf{E}}| = |-j\bar{\mathbf{K}} \times \bar{\mathbf{H}}|$$

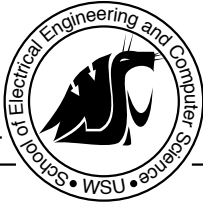
Because $\bar{\mathbf{K}}$ and $\bar{\mathbf{H}}$ are orthogonal and all fields have same spatial dependence, this becomes:

$$\Omega\epsilon|\bar{\mathbf{E}}_0| = |\bar{\mathbf{K}}| |\bar{\mathbf{H}}_0|$$

From dispersion relation $|\bar{\mathbf{K}}| = \sqrt{\epsilon\mu}\Omega$. Thus,

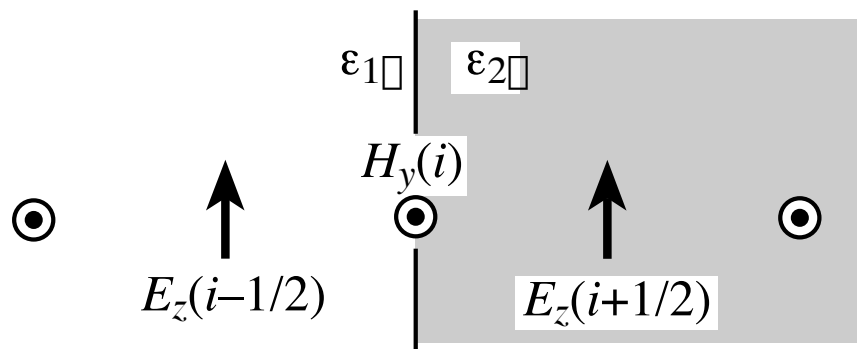
$$\frac{|\bar{\mathbf{E}}_0|}{|\bar{\mathbf{H}}_0|} = \frac{E_0}{H_0} = \sqrt{\frac{\mu}{\epsilon}}$$

Grid characteristic impedance is exact independent of direction of propagation.



Reflection Coefficient

Consider plane wave normally incident on planar interface:



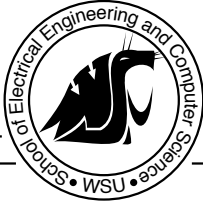
Assume incident, reflected, and transmitted electric field.

Via update equation, can express H at interface in terms of neighboring E 's.

H related to E via impedance relation. “Boundary condition” implied by H being common to medium 1 and 2:

$$\frac{1}{Z_1} [1 - \tilde{r}] = \frac{1}{Z_2} \tilde{T}$$

Combine and solve for reflection coefficient \tilde{r} .



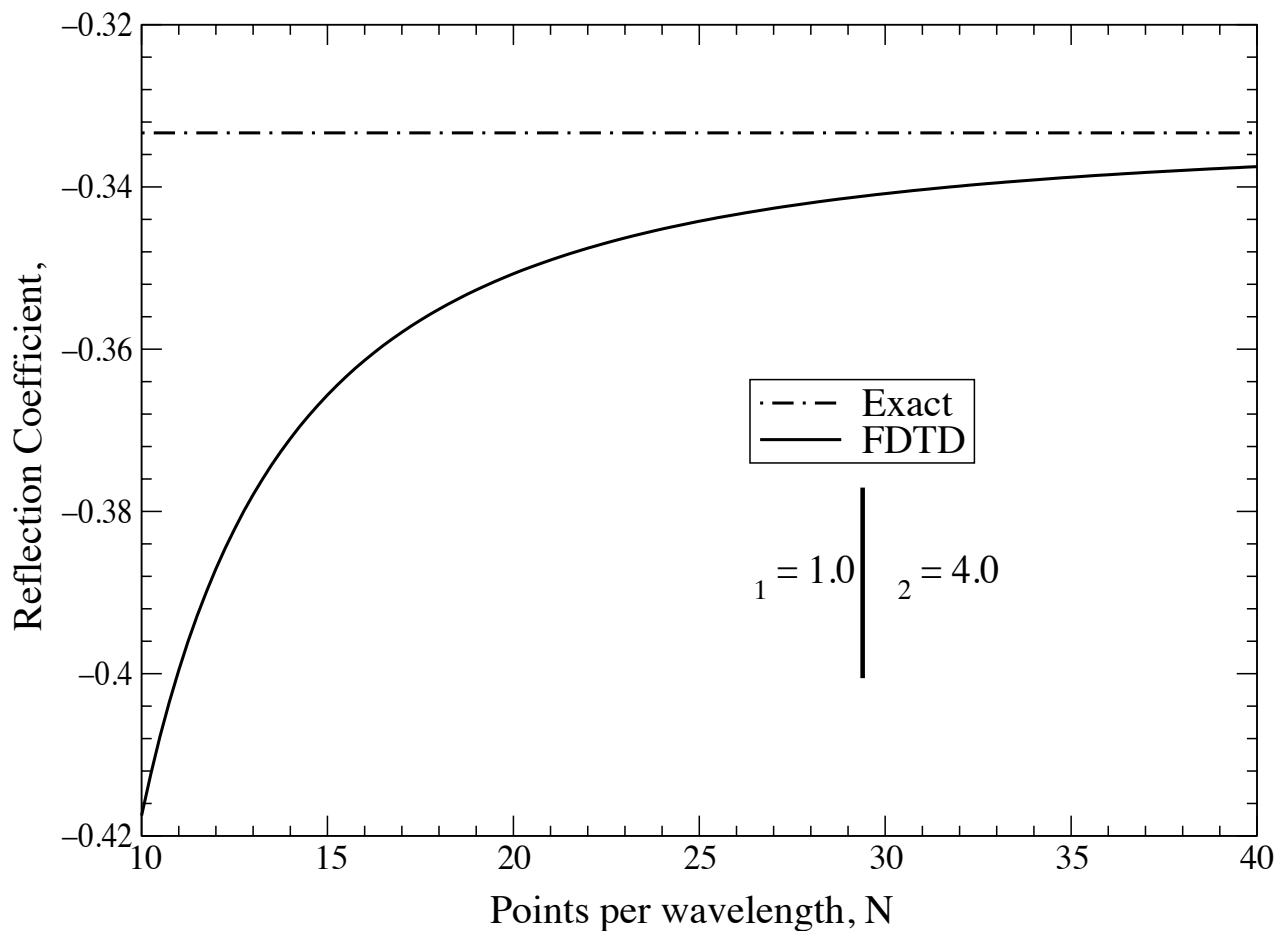
Reflection Coefficient (cont.)

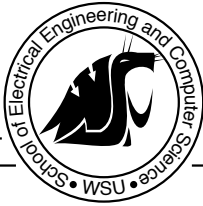
Solving for $\tilde{\Gamma}$ yields

$$\tilde{\Gamma} = \frac{\epsilon_1 \cos\left(\frac{\tilde{k}_2 \Delta x}{2}\right) - \epsilon_2 \cos\left(\frac{\tilde{k}_1 \Delta x}{2}\right)}{\epsilon_1 \cos\left(\frac{\tilde{k}_2 \Delta x}{2}\right) + \epsilon_2 \cos\left(\frac{\tilde{k}_1 \Delta x}{2}\right)}$$

Compare to continuous world:

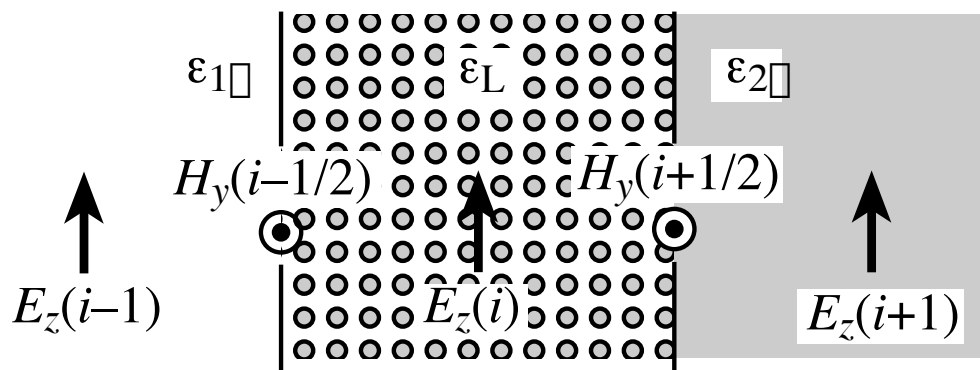
$$\Gamma = \frac{\epsilon_1 - \epsilon_2}{\epsilon_1 + \epsilon_2}$$





Reflection Coefficient—One Cell Layer

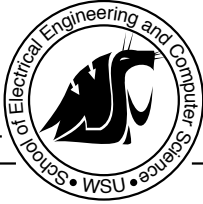
Plane wave normally incident on planar interface:



Solving for $\tilde{\Gamma}$ yields

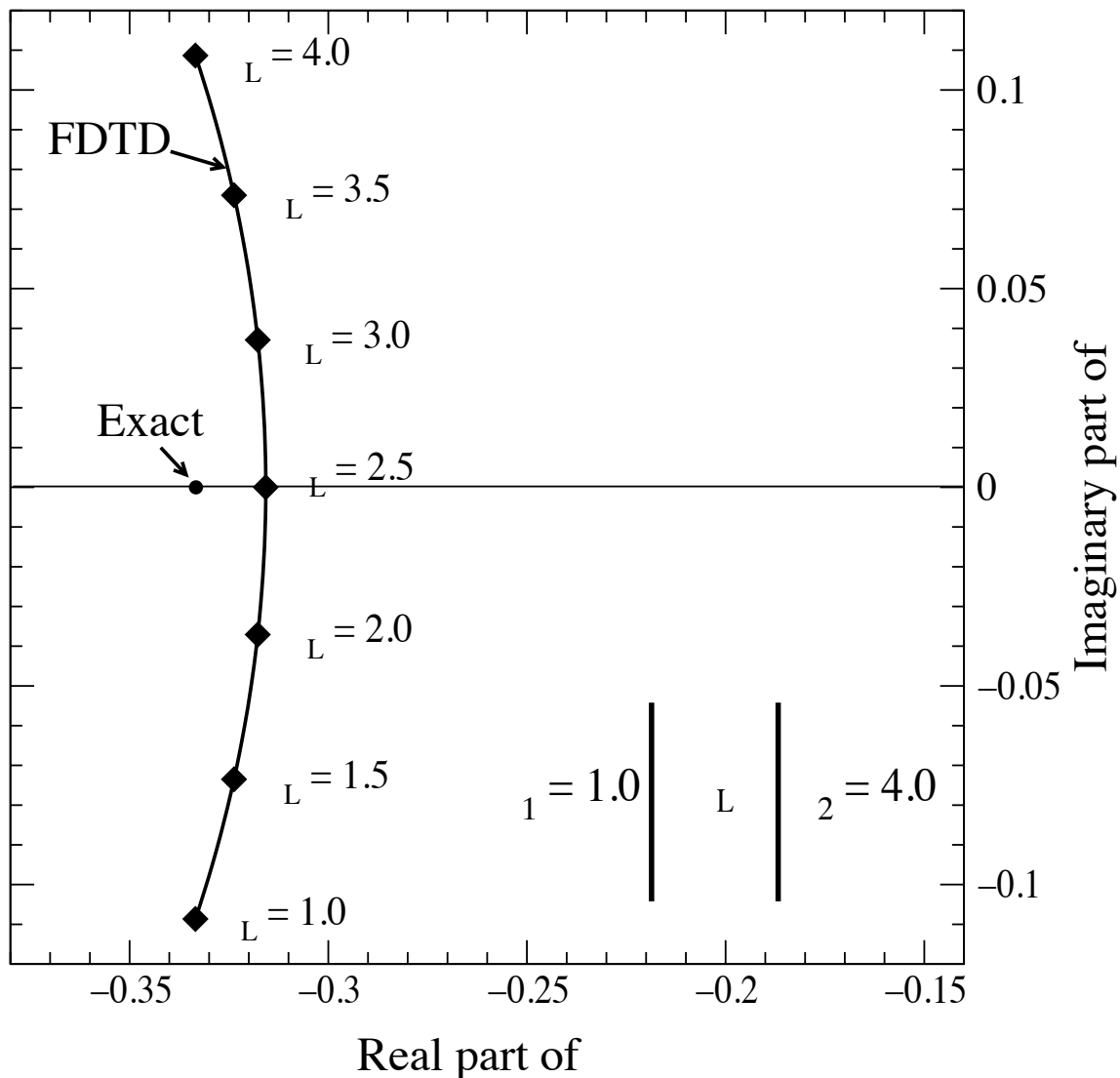
$$\tilde{\Gamma} = e^{j\tilde{k}_1\Delta x} \frac{\tilde{\Gamma}_{1L} + \tilde{\Gamma}_{L2} \exp(-j2\tilde{k}_L\Delta x)}{1 + \tilde{\Gamma}_{1L}\tilde{\Gamma}_{L2} \exp(-j2\tilde{k}_L\Delta x)}$$

where $\tilde{\Gamma}_{1L}$ and $\tilde{\Gamma}_{L2}$ are single-interface reflection coefficients.



Reflection Coefficient vs. Layer Permittivity

Let $\epsilon_1 = 1$ and $\epsilon_2 = 4$. What is optimum ϵ_L ?

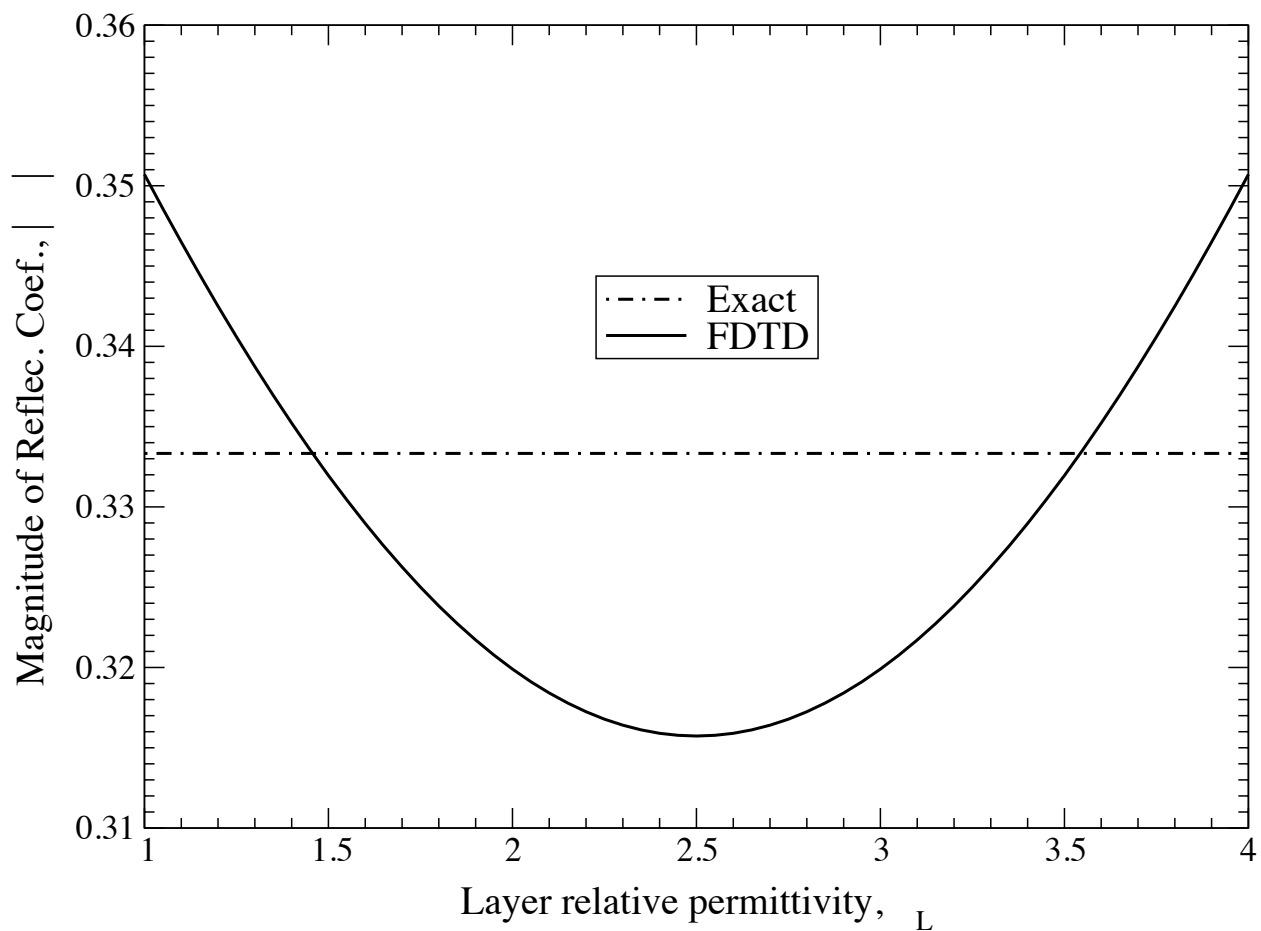


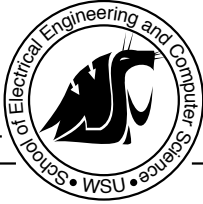
Optimum value = average of permittivities
to either side



Reflection Coefficient vs. Layer Permittivity (cont.)

Considering only magnitude of reflection coefficients will lead to wrong conclusions. For example:

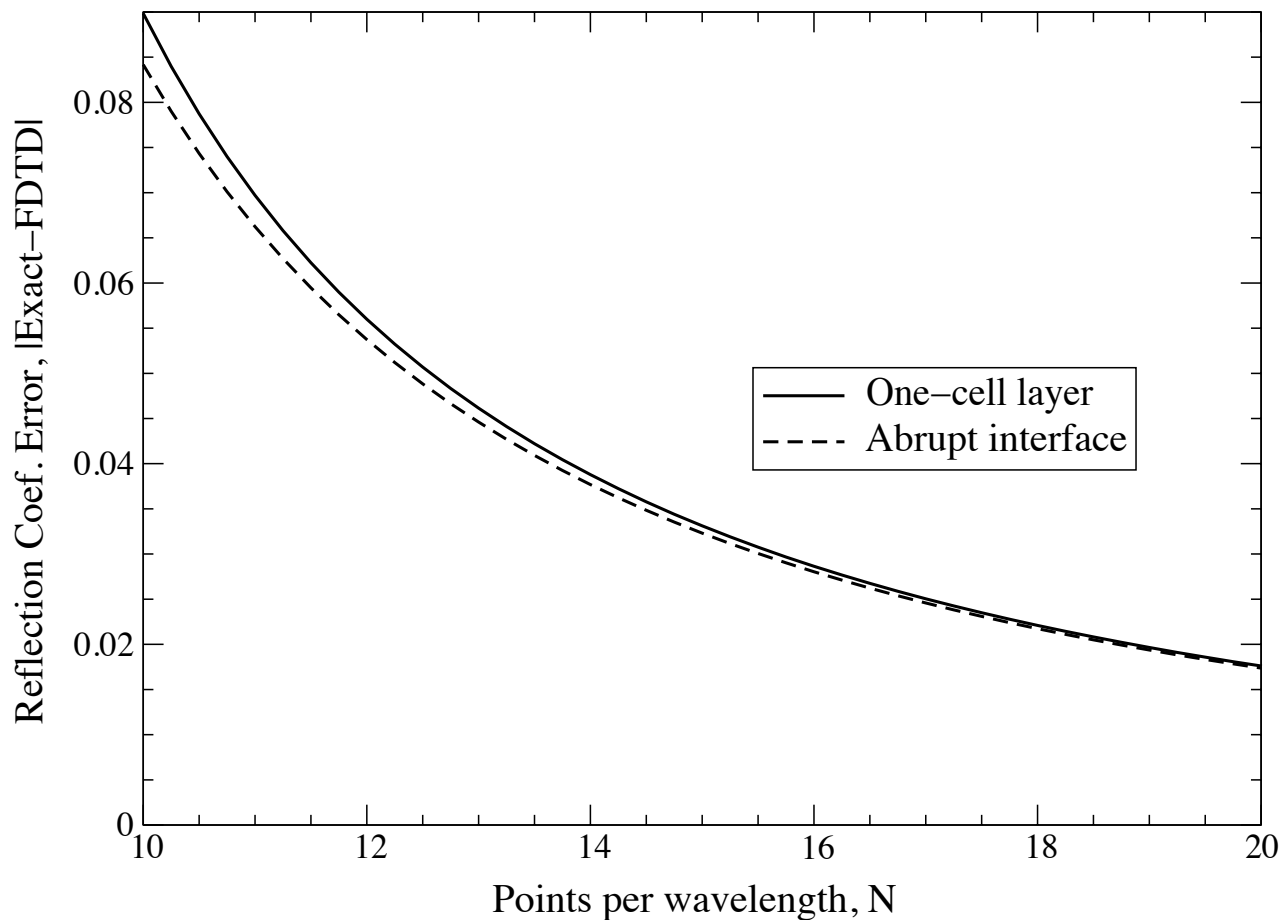




Abrupt Interface vs. One-Cell Layer

Error vs. points per wavelength for abrupt or layered realization of interface.

$$\epsilon_1 = 1.0 \quad (\epsilon_L = 2.5) \quad \epsilon_2 = 4.0$$



Abrupt realization of boundary superior (slightly) to layered one.

Additional Remarks

- Have derived reflection & transmission coefficients for obliquely incident waves.
 - TE and TM polarization
 - Layered and abrupt boundaries
- Have derived reflection coefficients for changes in permittivity and permeability.
 - Results depend on order in which discontinuities introduced.
- Have performed numerical simulations to confirm analytic results.

Conclusions

- $\bar{\mathbf{E}}$, $\bar{\mathbf{H}}$, and $\tilde{\mathbf{k}}$ are not mutually orthogonal
 - $\bar{\mathbf{E}}$, $\bar{\mathbf{H}}$, and $\bar{\mathbf{K}}$ are orthogonal
 - Second-order dependence for angle between $\bar{\mathbf{K}}$ and $\tilde{\mathbf{k}}$
- Characteristic impedance exact for all angles of propagation
- Reflection coefficient from planar boundaries can be analyzed via harmonic techniques
 - Reflection coefficient error dependent on discretization in both (all) media
 - Average permittivity is optimum when layered realization required
 - Abrupt realization slightly better than layered

Postscript

- Upcoming MGWL by Hirono *et al.* considers slightly different problem (geometric mean for “normal” permittivities optimal when boundary offset from grid-aligned position).
- Because $\bar{\mathbf{E}}$, $\bar{\mathbf{H}}$, and $\tilde{\mathbf{k}}$ not mutually orthogonal, may not make sense to study general 3D problems in terms of TE and TM polarization.